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Optimization of multilayer composite for solid rocket motor case using genetic algorithm

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Abstract:

The solid rocket motor (SRM) case of anti-tank weapon has been selected for this work. The structural analysis of the origin SRM under the maximum pressure 18.57 MPa, and thrust of the motor 1254 N, made by ANSYS workbench. The results shown that the safety factor of this case is 1.72. The SRM tube was then replaced with carbon fiber epoxy resin, and the design modified to hold the maximum pressure. The layup angles for composite tube found using Ansys direct Optimization, jointed with structural analysis using ANSYS ACP, show that the safety factor for composite is 2.63, and the ply sequence found by the optimization is ($\pm 40, \pm 50, \pm 4, \pm 76, \pm 28, \pm 66, \pm 63, \pm 87, \pm 44, \pm 88, \pm 28$). As expected the weight of the SRM composite tube is less than metallic tube, which was one third of the metallic one.

Key words: carbon fiber, epoxy resin, solid rocket motor case

1. INTRODUCTION

Due to low weight, high strength to weight ratio [1], and high corrosion resistance [2] compared with metallic materials, composites are widely used in aerospace, automotive, chemical

industries, marine, sport equipment and many other products and applications $[\underline{3}]$.

In the middle of 60th composite winding technology, introduced to solid rocket motor (SRM) cases manufacturer. In 1970 DuPont discovered the aramid fiber Kevlar, which stronger than fiberglass, and nylon fiber [4]. In 1980th carbon fiber has been discovered with mechanical properties and density superior to those of Kevlar. From that time and then, advanced composites become the most desirable material for rockets and missiles. Generally, SRM composite cases are useful to increase the ranges of missiles due to the gain of load comparable with maraging steel and titanium.

In 1984, graphite, and Kevlar 49 fiber, and LRF 092 resin system used for motor case of Sentry Initial propulsion Test Vehicle (IPTV) [5]. In 1993, Rafoss AS and MAN used intermediate modulus (IM) carbon fiber with a hot cured epoxy resin in a motor case for the Air-to-Air missile [6]. Now days there are numerous types of carbon fibers, which are recognize carbon fibers due to the precursors, or to the ultimate strength and young modulus.

In this work, a metallic rocket motor case replaced with a composite one. The selected materials are carbon fiber as reinforcement, and multi-functional novalac epoxy as a matrix. Ansys Composite PrepPost (ACP), and Ansys static structure, were used for structural analysis. Tsai Hu failure criterion selected as failure mod. The main goal of this study is to optimize the angles for each ply using Ansys direct optimization (DO)

2. MODELING AND SIMULATION

2.1 Metal case model

The SRM case of an anti-tank ammunition was selected for this study. Figure 1 represents the main dimensions of a 2D drawing of this SRM. The main parts of this SRM are: SRM

tube, nozzle, and adapter (Figure 2). Table 1 represents the materials, and mechanical properties attached to each part. From the SRM static firing test, the maximum pressure, and thrust obtained, were 18.57 MPa, and 1254 N respectively as shows in Figure 3. Geometry, Static structural within Ansys workbench were used to analyze the metallic SRM. The maximum pressure applied to the tube wall and the convergence part of the nozzle. The pressure applied to the nozzle throat, and to the divergence part of the nozzle about 0.54 of the maximum pressure [7]. The maximum thrust applied to the front of the SRM (Figure 4)



Figure 1 Tow dimensional drawing for the solid rocket motor (SRM)



Figure 2 SRM main parts



Figure 3 SRM Pressure and Thrust vs. time from static firing test

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Figure 4 Applied pressure and force to the SRM

Property	Tube Steel 4140	Nozzle Steel 5140	Adapter Al 7075
Density [kg/m ³]	7850	7850	2800
Young's Modulus, E [GPa]	210	200	71
Poisson's Ratio, v	0.3	0.3	0.33
Yield Strength, σ _{y0.02} [MPa]	650	800	503
Ultimate Tensile, σ_T [MPa]	1000	1200	573

2.2 Composite case model

The steel tube of the SRM replaced with composite material consist of around 60% carbon fiber and 40% epoxy resin. High strength moderate modulus carbon fiber and multifunctional novalac epoxy used for SRM tube. Table 2 Mechanical properties of SRM composite tube represents the properties of the composite material.

The design of the SRM modified in order to hold the gases pressure especially in the connecting parts of nozzle and the rear part with the tube. The maximum thickness of the tube become 5.5 mm instead of 1.5 mm the connected metallic part become inside the tube, which were outside in the original design. Even with this increase in the thickness of the tube wall, the composite tube is still lighter than the metallic tube, which is about the third of the metallic one (Figure 5 and Figure 6).

The tube divided to three parts, the mean tube, nozzle and adapter connections. The angles ranges for optimization which for 11 plies ($\pm \theta$) from the top. These 11 plies for the tube with thickness 5.5 mm. The target of optimization is to maximize the safety factor using Tsai Wu failure criteria.

Modeling of Composite layup made by Ansys ACP preprocessing. The nozzle and adapter solid parts modeled by mechanical modeler. The combination of the whole system done in static structural, then the internal pressures, and thrust, were similar to the metallic RSM added to the model and solved. The composite tube was then analyzed in Ansys ACP post-processing.

Ansys direct optimization (DO) – MOGA- used to get the optimum ply angles for each layer. From Ansys preprocess the ply angles assigned as input parameters, while the Reserve Factor (RF) assigned to be the main output parameter. Maximization of RF is main purpose of this optimization. The required RF for this application not less than 1.5. For optimization purposes, the ply angle set to be from 0° to $\pm 90^{\circ}$.



Figure 5 the modified RSM with composite tube 1. Composite case 2.Nozzle 3. Rear closure 1 4. Rear closure 2 5. Rear closure



Figure 6 Modeled modified RSM in Ansys

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Table 2 Mechanical properties of SRM composite tube				
Density [kg/m ³]	1540			
Longitudinal Young's Modulus, E1 [GPa]	170			
Transverse Young's Modulus, E ₂ [GPa]	8			
Poisson's Ratio, U12	0.28			
Poisson's Ratio, u23	0.4			
Tensile Strength, oT1 [MPa]	2700			
Tensile Strength, σ _{T2} [MPa]	50			
Compression Strength, σ_{c1} [MPa]	1600			
Compression Strength, σ_{c2} [MPa]	150			
In-plain shear strength, t ₁₂ [MPa]	60			
Out –off –plain shear strength, τ_{12} [MPa]	60			

3. RESULTS AND DISCUSSIONS

3.1 Metallic RSM

The metallic RSM experienced about 325 MPa maximum stresses (Figure 7). The maximum stresses appear in the convergence part of the nozzle, and this may related to the relatively high pressure applied. The actual pressure of the nozzle convergence gradually decreased starting of the pressure of the combustion chamber, to the throat pressure. The safety factor about 1.721 which acceptable for this working RSM. Table 3 shows these results.

Table 3 metallic SRM structural results	
Maximum equivalent (Von - Mises) stress [MPa]	325.31
Maximum equivalent elastic strain [mm/mm]	0.0026
Maximum total deformation (mm)	0.1578
Safety factor	1.721



Figure 7 Equivelant von-Mises stress along the SRM

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3.2 Composite RSM Optimization Results

The results of the optimization of the composite of the SRM showed in Figure 8,

Figure 9, and

Table 4. The benefit of using fiber in the SRM, over metal, is that the SRM need the thickness needed in longitudinal is actually the half of the thickness of circumferential, and this result of extra weight made generally by isotropic material. On the other hand fibers orientation solve this problem, and this clear on the results obtained by optimization, in which case the ply angles distribute between hope and longitude of the tube. Three layers lie around the angle $\pm 45^{\circ}$, which mean equally stresses distribution, and one angle near zero ($\pm 4^{\circ}$) serve the longitudinal stresses. For $\pm 4^{\circ}$ mainly is not applicable for winding machine but 7° to 10° will do the job. The other 7 layers above 60° and up to near 90° serve the hope stresses. The reserve factor RF, which represent the safety factor of the system, is above 2.6 for the three candidate results represented in

Table 4. Comparing this result with required value for such application 1.5, that more than required.

The weight gain, around two third of the metallic tube, will support the propulsion effort for the missile specially in large missile, in that case the using of composite material become must.



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Figure 8 the reserve factor stabilazation during optimaization

Table 4 the optimum ply angles candidates (degree)

	candidate #1 ($\pm \theta$)	candidate #2 ($\pm \theta$)	candidate #3 ($\pm \theta$)
P1 - ModelingPly.1.ply_angle	40.82	40.82	40.82
P3 - ModelingPly.3.ply_angle	50.79	46.69	50.87
P5 - ModelingPly.5.ply_angle	4.22	4.21	4.23
P7 - ModelingPly.7.ply_angle	76.56	76.56	76.5
P9 - ModelingPly.9.ply_angle	28.46	28.45	28.6
P11 - ModelingPly.11.ply_angle	66.28	66.28	75.43
P13 - ModelingPly.13.ply_angle	63.74	63.74	63.73
P15 - ModelingPly.15.ply_angle	87.68	87.25	87.04
P17 - ModelingPly.17.ply_angle	44.07	44.01	43.69
P19 - ModelingPly.19.ply_angle	88.55	88.39	88.39
P21 - ModelingPly.21.ply_angle	28.78	28.83	28.83
P46 - RF	2.63	2.63	2.62



Figure 9 the optimized angles of 11 layers of 22 layers; the other 11 lay layers take the negative values CONCLUSION

In this work, Ansys work bench component, Ansys ACP, and Ansys static structure was used for the structural analysis for the solid rocket motor (SRM). The SRM design was then modified in order to hold the SRM working pressure, which is about 18.57 MPa without losing the benefit of weight gain given by composite material over metallic material. The weight of the composite tube around one third of the metallic tube. The direct optimization using a genetic algorithm was then used to find the optimum ply angles, which maximize the reserve factor

(RF). The required RF for this application is 1.5, by using optimization the RF found around 2.6, and this optimization was converge after more than 500 of generated population over 11 parameters which were the ply angles. The optimization of ply angle generated different ply angles value which is different from usual ply staking where maximum two or three orientation angles were used among all layers. Now days the flexibility of winding machines make it easy to handle with different ply angles sequence which introduce much efficiency.

REFERENCES

[1] Park JS, Hong CS, Kim CG, Kim CU. Analysis of filament wound composite structure considering the change of winding angles through the thickness direction. Composite Structures. 2002;55:63-71.

[2] Bakaiyan H, Hosseini H, Ameri E. Analysis of multi-layered filament-wound composite pipes under combined internal pressure and thermomechanical loading with thermal variations. Composite Structures. 2009;88:532-41.

[3] Hung PL. Investigation of The Stability of Metallic/Composite-Cased Solid Propellant Rocket Motors under External Pressure [Dissertation]. Virginia Virginia Polytechnic Institute and State University, 1998.

[4] Peters ST. Composite filament winding. Materials Park: ASM International, 2011.

[5] Maheshwari M, Grover RL. Development of an Advanced Composite Rocket Motor Case for Internal and External Load Environments. AIAA/SAE/ASME 20th Joint Propulsion Conlerence. Cincinnati, Ohio: American Institute of Aeronautics and Astronautics (AIAA); 1984. p. 1 - 8.

[6] Fossumstuen K, Raudsandmoen G, Wurtinger H. Design Verification Programme for an Air-to-Air Type Rocket Motor with CFRP Composite Case and Reduced Smoke Propellant.

AIAA / SAE/ASME/ASEE 29th Joint Propulsion Conference and Exhibit. Monterey, Calafornia: American Institute of Aeronautics and Astronautics (AIAA); 1993. p. 1 - 12.

[7] Sutton GP, Biblarz O. Rocket propulsion elements. 8th ed. Hoboken, N.J.: Wiley, 2010.